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BASE 04 Transmission Loss Measurement and Modelling

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Contract Number: W7707-05-3094

Contract Scientific Authority: J. Theriault, 902-426-3100 ext 376

xwave Contract Number: 1010610

Defence R&D Canada – Atlantic

Contract Report
DRDC Atlantic CR 2006-108
October 2006

Canada

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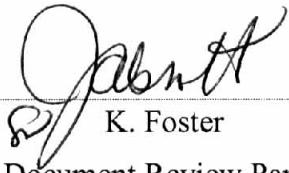
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Abstract

A previous contract resulted in the addition of the ray theory program Bellhop to the reverberation inversion program BREVER. This was done to allow inversion of reverberation results calculated from acoustic data recorded during the BASE 04 trials. However tests with Bellhop using parameters from the BASE 04 site indicated shortcomings in that program.

The current contract began with test runs of CASS, a potential Bellhop replacement for reverberation inversions. The test results indicated that CASS would work properly for the analysis area. Accordingly, BREVER was enhanced to allow it to also use CASS, and reverberation inversion was performed. The inversion results were used to model transmission loss, and these modelled values were compared to transmission loss data calculated from measured data.

Because of this contract the BREVER User's Guide was expanded to describe the use of the CASS-enabled version of the program.

Résumé

Dans le cadre d'un contrat antérieur, le programme de théorie des rayons Bellhop a été ajouté au programme d'inversion des réverbérations BREVER. Cet ajout avait pour but de permettre l'inversion des résultats de réverbérations établis à partir des données acoustiques enregistrées durant les essais BASE 04. Les essais effectués avec Bellhop à partir des paramètres de l'emplacement BASE 04 ont toutefois fait ressortir des lacunes de ce programme.

La mise en application du contrat actuel a commencé par des essais de CASS, solution possible de remplacement de Bellhop pour les inversions de réverbérations. Les résultats de ces essais ont indiqué que CASS fonctionnerait correctement pour l'analyse. Le programme BREVER a donc été adapté afin de pouvoir aussi utiliser CASS, et l'inversion des réverbérations a été exécutée. Les résultats de l'inversion ont servi à modéliser l'affaiblissement de transmission, et les valeurs modélisées ont été comparées aux données d'affaiblissement de transmission établies à partir des données mesurées.

À la suite de ce contrat, on a complété le guide de l'utilisateur de BREVER en décrivant l'utilisation de la version du programme faisant appel à CASS.

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Executive Summary

Introduction

The SWAMI suite of programs in use at DRDC Atlantic enables a user to produce modelled reverberation time series data based on a series of input parameters that describe the acoustic parameters of an area of a seabed. The modelled data can be compared to recorded reverberation data and a quantitative measurement can be made that essentially tests the goodness of fit of the modelled data to the measured values.

A previous contract resulted in the addition of the ray theory program Bellhop to the reverberation inversion program BREVER. This was done to allow inversion of reverberation results calculated from acoustic data recorded during the BASE 04 trials. However tests with Bellhop using parameters from the BASE 04 site indicated shortcomings in that program.

Results

The current contract began with test runs of CASS, a potential Bellhop replacement for reverberation inversions. The test results indicated that CASS would work properly for the analysis area. Accordingly, BREVER was enhanced to allow it to also use CASS, and reverberation inversion was performed. The inversion results were used to model transmission loss, and these modelled values were compared to transmission loss data calculated from measured data.

Significance

This effort lends itself to two particular applications. The first is Rapid Environmental Assessment (REA) using “through-the-sensor” techniques. The methodology extracts geoacoustic parameters from reverberation time series, one of the many goals of REA. The second application is in the development of Tactical Decision Aids (TDA). Real-time sonar performance estimation using in-situ measurements would provide the sonar operator with the capability to better employ the sensor.

Future plans

An effort to invert a larger reverberation data set measured by DRDC Atlantic’s Towed Integrated Active-Passive Sonar (TIAPS) is underway. Furthermore, a new energy function will be developed which will be less sensitive to errors in system calibration.

Calnan, C. 2006. *BASE 04 Transmission Loss Measurement and Modelling*, DRDC Atlantic CR 2006-108. Defence R&D Canada – Atlantic.

Sommaire

Introduction

La suite de programmes SWAMI utilisée à RDDC Atlantique permet à un utilisateur de produire des données modélisées de séries temporelles de réverbérations basées sur une série de paramètres d'entrée décrivant les paramètres acoustiques d'une zone du fond marin. Les données modélisées peuvent être comparées aux données de réverbérations enregistrées, et une mesure quantitative peut être effectuée pour évaluer essentiellement la qualité de l'ajustement des données modélisées aux valeurs mesurées.

Dans le cadre d'un contrat antérieur, le programme de théorie des rayons Bellhop a été ajouté au programme d'inversion des réverbérations BREVER. Cet ajout avait pour but de permettre l'inversion des résultats de réverbérations établis à partir des données acoustiques enregistrées durant les essais BASE 04. Les essais effectués avec Bellhop à partir des paramètres de l'emplacement BASE 04 ont toutefois fait ressortir des lacunes de ce programme.

Résultats

La mise en application du contrat actuel a commencé par des essais de CASS, solution possible de remplacement de Bellhop pour les inversions de réverbérations. Les résultats de ces essais ont indiqué que CASS fonctionnerait correctement pour l'analyse. Le programme BREVER a donc été adapté afin de pouvoir aussi utiliser CASS, et l'inversion des réverbérations a été exécutée. Les résultats de l'inversion ont servi à modéliser l'affaiblissement de transmission, et les valeurs modélisées ont été comparées aux données d'affaiblissement de transmission établies à partir des données mesurées.

Portée

Ces travaux se prêtent à deux applications particulières. La première est celle de l'analyse environnementale rapide (REA) au moyen de techniques de détection. Cette méthode consiste à extraire des paramètres géoacoustiques des séries temporelles de réverbérations, soit l'un des nombreux objectifs de la REA. La seconde application a trait au développement d'aides à la prise de décisions tactiques (TDA). L'évaluation en temps réel du rendement d'un sonar à partir de mesures sur place permettrait à l'opérateur du sonar de faire un meilleur usage du détecteur.

Recherches futures

Des travaux en cours visent à inverser un plus vaste ensemble de données de réverbérations, mesurées au moyen du sonar actif-passif intégré remorqué (TIAPS) de RDDC Atlantique. Par ailleurs, on mettra au point une nouvelle fonction relative à l'énergie, qui sera moins sensible aux erreurs d'étalonnage du système.

Calnan, C. 2006. *BASE 04 Transmission Loss Measurement and Modelling* (Mesure et modélisation de l'affaiblissement de transmission de BASE 04) RDDC Atlantique CR 2006-108. R & D pour la défense Canada – Atlantique.

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1. Introduction

Contractor Report [1] describes the expansion of the reverberation inversion program **BREVER** to allow it to use the ray theory program **Bellhop**. More importantly as it relates to the current report, Section 5 of that report describes how **Bellhop** could not operate properly under the conditions of the BASE 04 trial area.

Following that discovery, the program **CASS** was tested and found to run correctly under the oceanographic conditions that exposed **Bellhop** deficiencies. (CASS – Comprehensive Acoustic System Simulation – is used at DRDC Atlantic by permission of its owner, the U.S. Navy’s Undersea Warfare Research Center.)

The reverberation inversion program **BREVER** [2] was then modified so it could use **CASS**, and inversions were performed based on reverberation data obtained by analysing a particular ping. The results of the reverberation inversion were geoacoustic parameters that provided a “best fit” of modelled reverberation results to the data produced by analysis.

These inverted geoacoustic parameter values were used to produce modelled transmission loss data, which were then compared to transmission loss results calculated from measured data.

Besides common English typographic conventions, the following conventions are used in this document:

- **bold text** is used for filenames (e.g. **test.pro** or **/local/files/test.pro**)
- **bold italics text** is used for directories (e.g. **/usr/tmp**)
- *italics text* is used for computer and program suite names (e.g. *Tessie* and *DMOS*)
- **Bold Arial text** is used to indicate program names (e.g. **BREVER**, **Bellhop**)
- Arial text is used to indicate function and subroutine names (e.g. **PPR_SETUP**)
- *italic Arial text* is used for variables’ names in computer programs or associated with operating systems (e.g. *IDL_PATH*)
- **Courier text** is used for text to be typed on the keyboard, code or file listings, etc. (e.g. enter “**idl**”)

2. BREVER Expansion

The requirement to use **CASS** as an alternative to the *DMOS* programs **PMODES** and **Bellhop** as **BREVER's** transmission loss model resulted in modifications to **BREVER**. And because **CASS's** operation was appreciably different from that of both **PMODES** and **Bellhop**, a fair amount of the **BREVER** code had to be rewritten so as to produce **CASS** input files of the appropriate format and contents.

While the code modification was underway, the reverberation analysis results produced by MDA (MacDonald, Dettwiler & Associates Ltd.) personnel became available and were closely examined. It was immediately realized that many, if not all, of the reverberations from the six beams were limited by background noise. This resulted in the decision to further modify **BREVER** to allow it either solve for an individual background noise for each beam, make use of a user-provided background noise for each beam, or solve for some and use provided values for others. This decision resulted in even more code modifications.

In reality the background noise along a beam is a combination of the effects from self noise within the recording hydrophones and environmental noise external to the devices, a combination that may be highly directional. For data analysis purposes, however, the sources of individual components of the noise and their magnitudes are irrelevant and only the sum of the noise in the beams' directions is important. Because these noises are of importance in each beam's direction, they are referred to in the **BREVER** user's guide [2] and this report as "beam noise."

A number of **CASS** input options were hard-coded into **BREVER**. These options were decided upon as being most likely to produce the best results for the cases under which **BREVER** would be running. The following table lists the options and their values exactly as entered in the **CASS** input file.

Table 1. Hard-Coded **CASS** Parameters

CASS Parameter	Parameter Value
EIGENRAY MODEL	GRAB
INTERPOLATION ORDER	LINEAR
RAY MODEL	TWO-DIMENSIONAL
COHERENCE	RANDOM
SEA STATE-WIND SPEED CONVERSION	NAVOCEANO
BOTTOM REFLECTION COEFFICIENT MODEL	RAYLEIGH
VOLUME ATTENUATION MODEL	THORP
OCEAN SOUND SPEED MODEL	LINEAR
BOTTOM SCATTERING STRENGTH MODEL	MACKENZIE
SURFACE REFLECTION COEFFICIENT MODEL	BECHMANN

2.1 New Program ER_CONV

BREVER runs **CASS** in such a way that it produces eigenray files. These files must be converted to *DMOS* eigenray format before subsequent programs (**MONOGO** and **EXCESS1**, for example) can make use of them. The Fortran 90/95 program **ER_CONV** (for eigenray conversion) was written to perform this task. The intent for this program is that it will eventually contain code to convert eigenray files (or files containing data that may be easily converted to eigenray files) from any number of sources from one format to another. At present **ER_CONV** can only convert **CASS** eigenray files to *DMOS* format, but the program was written to allow easy expansion as required.

BREVER's CASS-related modifications cause it to:

- create the input files needed by **CASS**,
- run **CASS**,
- create the input files needed by **ER_CONV**, and
- run **ER_CONV**.

Following the creation of *DMOS* format eigenray files by **ER_CONV**, processing continues as it did before.

3. Inversion Run Parameters

Once the data and the **CASS** and beam noise enabled version of **BREVER** was in place a number of reverberation inversion runs were made. The majority of the parameters involved with the inversion runs were identical, but a couple of the parameters were changed for each run.

Seven **BREVER** runs were made in all, but only three provided results quoted in this report: runs 4, 5, and 7. The other runs were either test runs, used incorrect data, or used data determined not to provide optimal results. In this report the runs will be referred to by their numbers as mentioned above and as used on *Spray* and *Pinta*, the computers used for the analyses.

It would have been simpler to call the runs described in this report 1, 2, and 3, but by keeping the original run numbers it is simpler to locate the data files on the computers used. On these machines the analyses were run in the directory `~calnan/projects/anal-1` (for analysis 1; there turned out not to be a second set of analyses). Input files and results were put into subdirectories off this named **run1**, **run2**, etc. In general input files were created on *Pinta*, analyses performed on the faster computer *Spray*, and results were later copied to *Pinta*.

The **run1**, **run2**, ... subdirectories often have subdirectories themselves named **rev** and **tl**. The former hold reverberation related files and the latter contain transmission loss data files.

3.1 Fixed Input Parameters

The parameters that are fixed on all inversion runs come under several categories:

- ping parameters, which are defined by the time and location that the ping was emitted and recorded;
- analysis choices pertaining to directions of interest; and
- inversion analysis parameters.

After examining the data recorded on June 1, 2004, MDA personnel identified a ping that was to be isolated and studied, and obtained the time it was emitted. This ping was produced by the VP2 and recorded by DASM (Directional Acoustic Sensor Module), both of which were towed by the *Quest*. The DASM NADAS data, recorded every minute, were examined to locate the position and velocity data that bracketed the ping's time. Linear interpolation was performed on the bracketing data to obtain the DASM's position, heading, and speed at the ping time. These values, along with DASM-specific parameters, are presented in the following table.

Table 2. Ping/DASM Parameters

Ping/DASM Parameter	Value
Date/Time	2004-06-01 12:26:40.092
Location	36° 18.317' N, 14° 43.154' E
Heading	018.0° True
Speed	2.5 m/s
Depth	66 m
Weighting	Square
Tilt	0 deg
Number of Receivers	94
Receiver Spacing	0.5 m
Weighting Parameter	1.0
Floor	-30 dB
Detection Threshold	-2.0
System Loss	3.0

The VP2 sound source was assumed to be in the same physical environment as the DASM. The parameters associated with the source are presented in the following table.

Table 3. Ping Source Parameters

Ping Source Parameter	Value
Source level	217 dB
Ping Frequency	1125 Hz
Bandwidth	50 Hz
Ping Length	1.5 s
Pulse Type	LFM

Based on the bathymetry of the area and the locations of potential targets, six directions were selected for study. These directions are listed in the following table, and it should be noted that the last three directions are mirror angles of the first three based on the heading of 018.0° True.

Table 4. Study Angles

Angle Number	Angle Bearing
1	057.6° T
2	090.8° T
3	119.8° T
4	276.2° T
5	305.2° T
6	338.4° T

Gridded bathymetry data of the area were provided by Dr. Sean Pecknold. As indicated by the grid point spacing, the resolution of the gridded data was approximately 111 m in the north-south direction and 135 m in the east-west direction. However, a number of areas of the gridded depth data repeated the same value over a number of points, so the actual resolution was, in places, less than that implied by the grid spacing. For the inversion bathymetry data were interpolated along the radial directions at 500 m intervals.

The following figure presents the bathymetry profiles along the study angles. In this diagram the bathymetry profiles that are mirror pairs about the bearing angle of the instruments are presented in the same colour. **BREVER** used the bathymetry as provided.

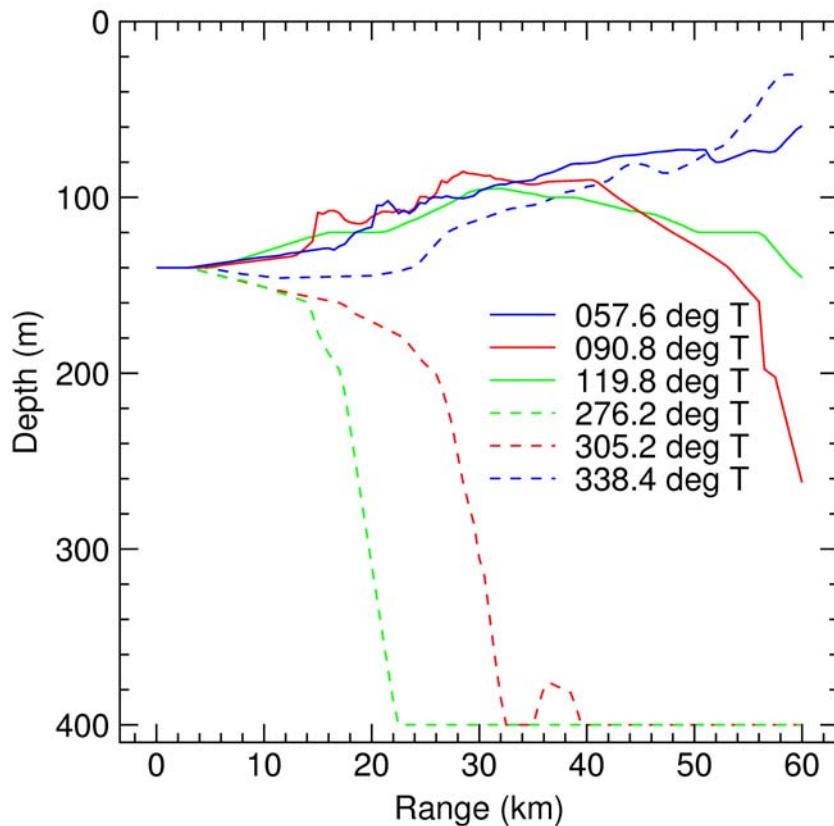


Figure 1. Bathymetry Profiles along Selected Radials

The list of sound speed profiles recorded on June 1, 2004 was examined and the one nearest to the DASM at the time of the ping, both geographically and temporally, was identified. This profile, T0_00036, was recorded in about 170 m of water approximately 200 m away from the DASM at a bearing of 020° T and 97 minutes after the ping. Two profiles were recorded closer to the time of the ping, but they were taken 9 and 17 km away from the DASM.

A subset of 20 values was extracted from T0_00036 to provide the sound speed profile to be used in modelling. This subset contained data located at the points where the sound speed changed, ignoring the ranges where the sound speed changed in linearly.

The profile data are displayed in the following figure with the extracted points used in the inversion displayed as small dark blue squares. Also presented in the figure is the depth of the transmitter and receiver.

To provide for sound speed data at depths greater than 170 m, a data point specifying 1516.5 m/s at 400 m was added to the profile. This value was extrapolated from the recorded data.

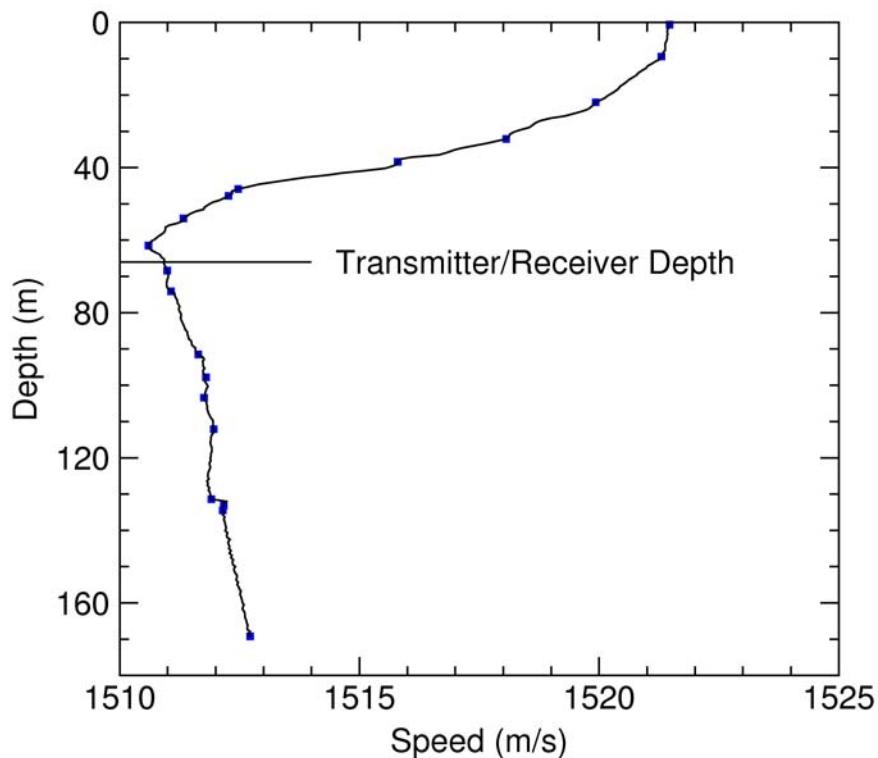


Figure 2. Sound Speed Profile

The bathymetry and sound speed profiles were used as input to **CASS** in order to produce a set of eigenrays for each radial.

Portions of all of the above data were used by MDA's personnel to analyse the recorded data and provide a reverberation time series at a data rate of 4096 Hz. These data were averaged over half-second intervals centred on the second and half-second

to provide a 2 Hz data set. This averaged time series was created to be the measured data set that **BREVER** would use for comparison with test data.

The final set of fixed parameters is the set of parameters put into **BREVER's** input file and left unchanged for all the inversion runs. The following table lists these data, following which are comments on why some of these values were chosen.

Table 5. Fixed BREVER Parameters

Parameter	Value		
ASSA Parameters:			
T0	Tfact	Ntemp	1.0 0.99 200
NPERT	NDHS	NAVE	5 70 20000
NPERTM	PVC	PVCmult	5 1 3.0
SSA Conv	DHS Conv		0.01 1.0E-4
Rev Wt	Slope Wt		1.0 0.05
Minimum range step size and delta (km)			
Eigenray angle range and step size			
Wind speed (kt)			
Maximum number of bottom bounces			

The numbers of temperature and downhill simplex quenching loops (“Ntemp” and “NDHS”) were set, respectively, to 200 and 70. Normally these values are set appreciably larger, for example to 1500 and 500, but the amount of time required for an inversion run is much larger when **CASS** is used over the other transmission loss models. Therefore, in order to have **BREVER** complete its runs in reasonable periods of time these numbers were set lower than normal. Despite reducing the size of the loop runs, several inversion runs took over two days to complete.

Two other parameters with values are those of the reverberation and reverberation slope weights (“Rev Wt” and “Slope Wt”). The relative values define if the inversion is more sensitive to the magnitude (Rev Wt) or the decay rate (Slope Wt) of the reverberation model-data differences. This feature must be used with caution. If ambient noise is included (as in the BASE '04 data), the constant level may dominate the time series and result in a meaningless geoacoustic parameterization.

3.2 Varying Input Parameters

Other parameters were varied between the three runs in order to see what would happen. The following table shows how the timing and radial parameters were changed from run to run.

Table 6. Varying BREVER Parameters

Parameter	Run 4	Run 5	Run 7
Minimum and maximum time (s)	4 and 39	2 and 10	4 and 39
Radial length (km)	30	8	30
Points per radial	11	17	11
Dist between radial points (km)	3.0	0.5	3.0
Beam Noise	Solved for	Solved for	Fixed

Run 4 was set up with timing and distance (as given via radial length) parameters set to match the timing/distance limits of the reverberation results produced by other personnel.

An examination of the Run 4 results indicated that the inversion results did not provide a very good fit to the measured data at small times. Consequently, Run 5 was devised to see if using shorter distances between radial points and a maximum time closer to zero would give a better fit for that portion of the data.

Run 7 was set up to mimic Run 4 with one important difference: whereas Run 4 solved for beam noise, estimates for these data were read off the plots of measured reverberation and were used as provided. This reduced the number of parameters that **BREVER** had to solve for and ensured that at least the background of the calculated reverberation would be realistic.

3.3 Parameters Solved For

The **BREVER** runs were set up to always solve for:

- bottom density
- bottom sound speed ratio, and
- bottom scattering strength.

In addition some runs also solved for beam noise. Of the runs described in this report, Runs 4 and 5 solved for beam noise and Run 7 used fixed beam noise values as input.

4. Reverberation Results

There are six figures in this section, with each presenting data related to one of the directions of interest, also known as beam angles. The figures display four curves each: the measured reverberation data for the beam along each direction and the inverted Run 4, 5, and 7 reverberations along the same bearings.

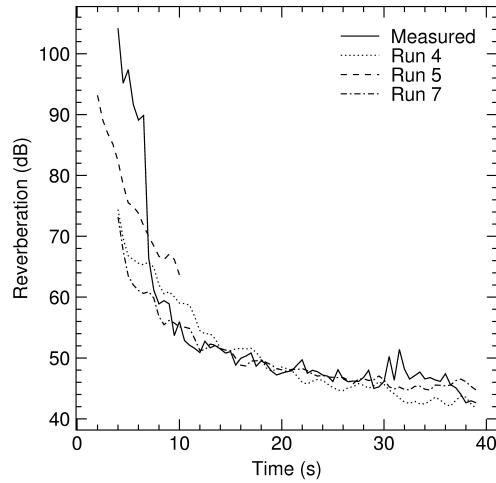


Figure 3. Beam 1 – 057.6° T

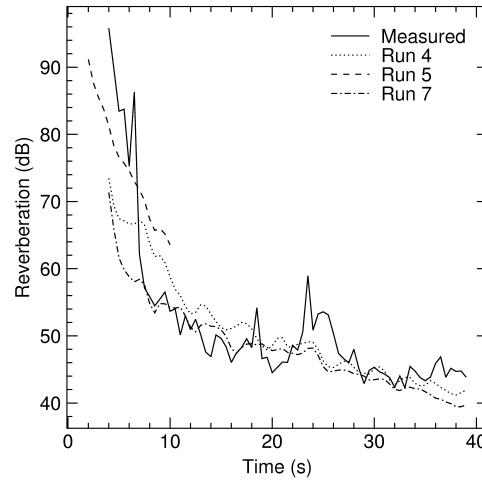


Figure 4. Beam 2 – 090.8° T

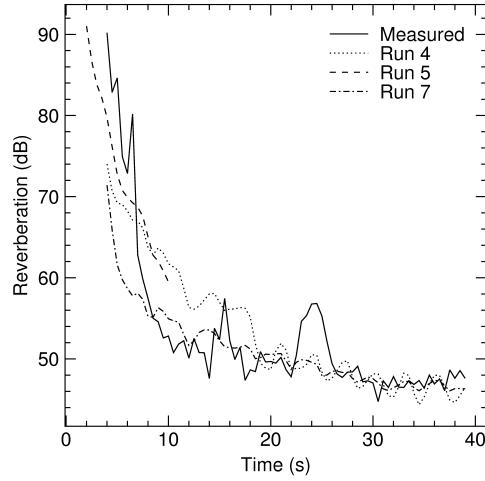


Figure 5. Beam 3 – 119.8° T

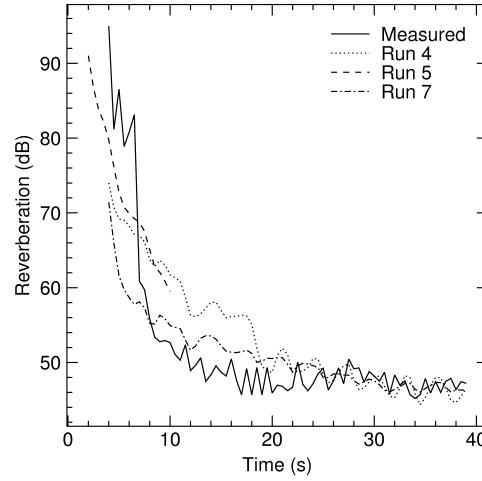


Figure 6. Beam 4 – 276.2° T

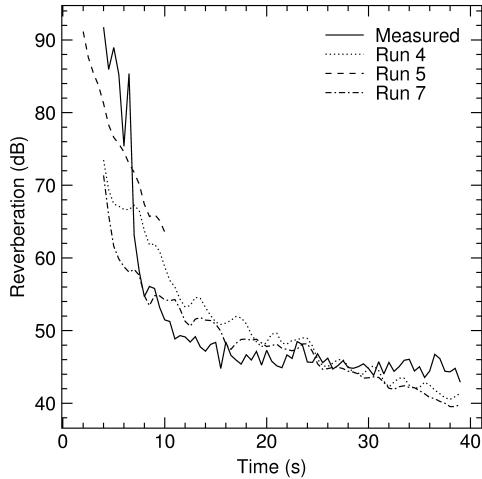


Figure 7. Beam 5 – 305.2° T

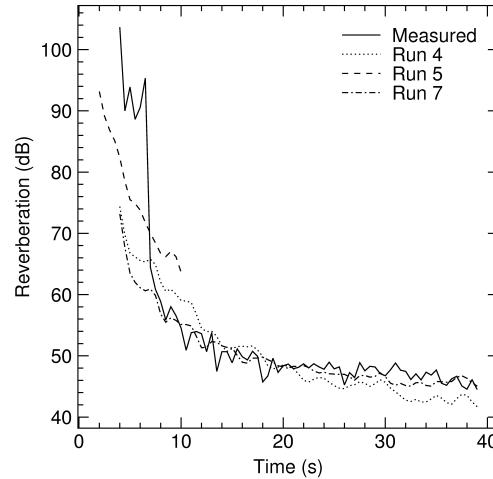


Figure 8. Beam 6 – 338.4° T

In all figures the shorter duration of the Run 5 inversion is apparent, as is the fact that it produces a better fit to the first 10 seconds of the measured data.

As well, Run 7, calculated with beam noise data assigned values read off the measured data curves, resulted in a curve that generally fits the measured data somewhat better than Run 4, which solved for the beam noise.

The longer duration runs, 4 and 7, do not match the measured data very well at times up to about 7 seconds, the time range over which the measured results have the greatest drop in reverberation. The reason for this is not known, although some possibilities are:

- the models used in the inversion may simply be unable to model this type of behaviour, regardless of input values,
- the timestep size of 0.5 s may be too large to allow the model to reach a better fit, or, more likely,
- the range step size being used in the inversion may be too large.

The latter two possibilities could be tested, either alone or in combination, but the inversion runs would take appreciable time to complete, time that is beyond what is available to the contract at this point.

5. Transmission Loss Modelling

This section describes how **BREVER** results were used to model transmission loss.

For this data analysis the **BREVER** runs were made using a directional transmitter and receiver, but the transmission loss files were to be made with omnidirectional equipment.

In each run's subdirectory (e.g. **run4**) the subdirectory **tl** was created. All files needed to create the run's transmission loss data were moved into these directories and all processing was performed in them.

The steps that were taken to produce the desired data are as follows.

1. The program **INTEGRATE** had to be run in order to produce new **.sys** files, and the first step was to run that program.

The **INTEGRATE** input file was edited to change the transmitter and receiver types to omnidirectional (i.e. **Omni.tx** and **Omni.rx**), but the program was allowed to use the same radials file.

Using a main input file named **integrate.input**, **INTEGRATE** was run with the command:

```
INTEGRATE < integrate.input > integrate.log
```

2. **CASS** had to be run to create new eigenray files. This was necessary because when being run by **BREVER**, **CASS** created eigenray files for the seabed, but to produce transmission loss data eigenrays are needed for the target depth. This depth was set ~5 metres off the source depth. In the current case the source was at 66 m, so a target depth of 60 m was chosen.

The other files needed by **CASS** are the bathymetry, **BAT***, and **BTM*** files, all of which contain the correct data at the end of a **BREVER** run as made during this analysis. However before making the run the file **cass_in.DAT** had to be edited. The lines that read “TARGET DEPTH = BOTTOM” were changed to contain “TARGET DEPTH = 60 M”. There was one such line per radial.

CASS only had to be run once to create eigenray files for all the radials, and this was done via the command:

```
CASS < cass.in > cass.log
```

3. **ER_CONV** had to be run once for each radial in order to convert the **CASS** eigenray file to **DMOS** format.

There are two main input files for **ER_CONV** for each radial. The first is

erc_in.NN (where *NN* is the radial number) and it simply contains the name of the other main input file. That second file is **erc_in.NN-pars**, and it contains the parameter data needed by the program. Both files were copied from the **BREVER** run, which created them when it ran.

All filenames were maintained so the files were used as is with one change: **erc_in.NN-pars** had its last line changed so that the target depth was changed from the default of 0.0 m to the actual target depth of 60.

The program was run once for each radial, and the command to run it for radial 2 is:

```
ER_CONV < erc_in.02 > ER_CONV_02.log
```

4. Transmission loss files were then created by running **EXCESS1** for each radial. This program needed a new main input file, which was created in a text editor. The following is the sample file **excess1_r04.input** created for radial 4 during Run 5, and it is followed by a listing of its contents by data line.

Listing 1. EXCESS1 Input File

BASE 04 - Run 5	
LT	!2 options: Long output and tl
BR5_2762.des	!3 Input Environ. Description
BR5_2762.sys	!4 Input System File
Target.des	!5 Input Target File
BR5_2762.tls	!6 Output TL File
0.5	!7 Range Minimum (km)
0.5	!8 Range Increment (km)
80	!9 Number of Range Points
276.2	!10 Sub-radial Minimum (deg)
0.	!11 Sub-radial Increment (deg)
1	!12 Number of Radial Points

Table 7. Contents of an INTEGRATE Input File

Data Line	Contents
1	Title (Generally ignored.)
2	The necessary options
3-6	The names of the appropriate input and output files.
7-9	Sets the number of points along the radial and their spacing.
10	The bearing of the radial.
11-12	Should be zero and one, unless something more sophisticated than the transmission loss along a specific bearing is desired.

The input file specified the target description file **Target.des**, which was also created in a text editor. The following listing presents the file that was used. Line 1 is a title and the rest is self-descriptive.

Listing 2. Target Description File

```
Example target
10          ! Target strength (dB)
1           ! No. target depths
60          ! Target depth (m)
```

An **EXCESS1** run also requires the presence of:

- the **.des** files, as named on data line 3 of the **EXCESS1** input file
- the bottom bathymetry files named in the main **BREVER** input file, and
- the sound speed profile file named in the main **BREVER** input file.

The **EXCESS1** run for the above input file was initiated with the following command:

```
EXCESS1 < excess1_r04.input > excess1_r04.log
```

Once **EXCESS1** had been run for all of the radials, a **SAPLOT** input file was created for the run using data from the transmission loss files named in data line 6 of the **EXCESS1** main input files. These files resulted in curves plotting the transmission loss for all radials.

The following section describes other data that were added to the **SAPLOT** files and presents the resulting plots.

6. Transmission Loss Results

This section contains one figure for each of the three inversion runs described in this report. They present the results of transmission loss modelling, as is described in the previous section, as a series of curves, one for each radial. The plots also contain actual transmission loss data calculated by Dr. Sean Pecknold from data recorded during the period around the time of the ping used. He documents the production of these transmission loss data points in [3].

There are two sources of the data analysed by Dr. Pecknold and each has its own symbol. The first series of pings were produced by equipment being towed by the research vessel *Alliance*. The setup of the trial involved having the *Quest* and the *Alliance* travelling towards each other, passing, and continuing in a straight line. All bypasses occurred near the centre of a petal-shaped pattern.

The second set of pings was produced by the DAP (Drifting Acoustic Projector). This device was free-floating near the centre of the petal-shaped pattern that both the *Alliance* and the *Quest* were crossing in opposite directions.

It must be pointed out that the *Alliance* and DAP data points each represent one ping while the lines produced by **EXCESS1** are based on reverberation data derived from one ping that was produced by another instrument. The *Alliance* and DAP transmission loss data points are the same in the three figures in this section.

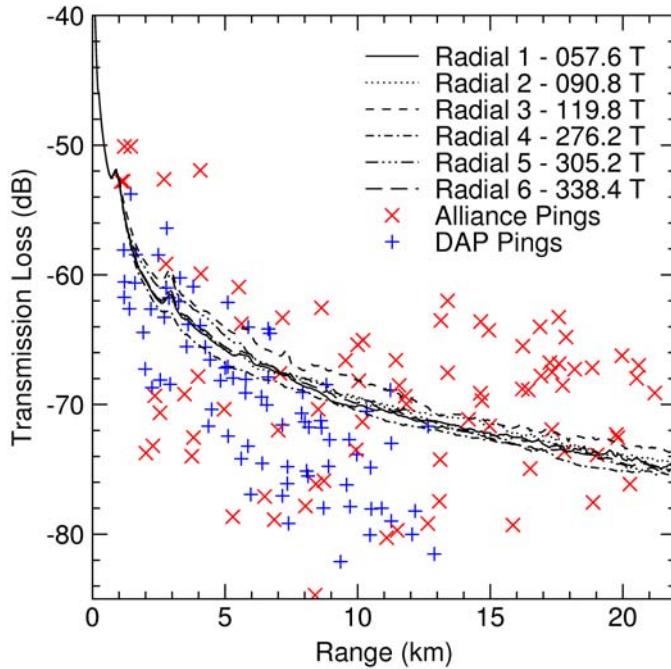


Figure 9. Run 4 Transmission Loss Results

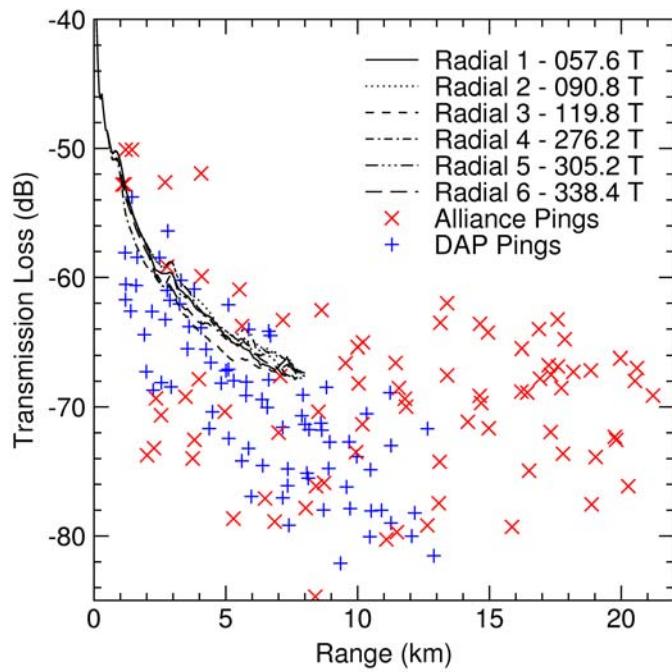


Figure 10. Run 5 Transmission Loss Results

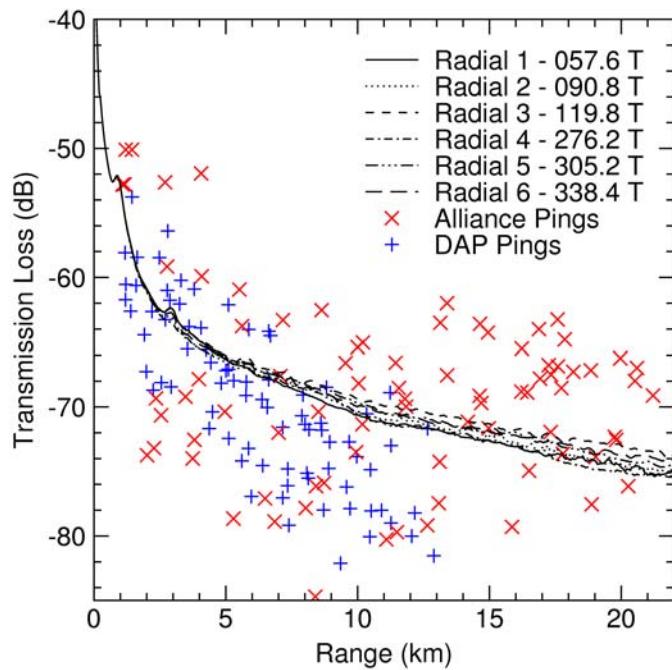


Figure 11. Run 7 Transmission Loss Results

The shorter radial length used in Run 4 is apparent in the plot of data from that inversion run. The other two runs were made out to 30 seconds, but the plots were clipped at 22 seconds since no observed values went past that time.

A few features can be determined from comparing the transmission loss plots.

- In all cases the modelled data are within the spread of the measured data.
- The spread of the Run 4 and 5 curves for the different radials is greater than that from Run 7.
- The Run 7 transmission losses are slightly lower than those of Run 4.

7. Conclusions and Discussion

The reverberation inversion results of the different runs produce reverberation data that follow the trend of the measured data to varying degrees. It is quite possible that using a higher number of points along the radials would provide a better fitting set of results, but this test was not made because of time limitations.

The main drop-off of measured data occurs at about seven seconds, which translates to a distance of about 5.3 km at a sound speed of 1515 m/s. Runs 4 and 7 used a 3 km radial point spacing, which would result in the first two points occurring before the drop-off and the rest of them occurring afterwards. This plateau effect may be difficult to model.

The Run 5 case, which used a radial point spacing of 500 m, produced a better fit to the close range measured data, but it's possible that an even shorter radial point interval would have resulted in a better fit.

As well, in all cases the time interval given to **MONOGO** for calculating the reverberation was 0.5 s, which is roughly equivalent to a spacing of 380 m. It may be that matching time intervals to radial point separations (or vice versa) might produce a more coherent analysis setup and so better results. This parameter matching also was not tested, in part due to time limitations.

The entire **BREVER** inversion process is directed towards to producing results that produce a fit to either measured reverberation data, the slope of these data, or a weighted combination of the two. Modelled transmission losses are calculated using geoacoustical parameter values obtained from the inversion, and as such are, in effect, completely independent of the inversion process. If it were possible to produce curves of transmission losses based on measured data, an analogue of **BREVER** could be created that performs an inversion that is directly based in transmission loss. This program, however, would not be attempting to fit modelled reverberation data to measured data, and so intermediate reverberation data would not be expected to fit measured reverberation data because none would be needed in this process.

However, a further variant of **BREVER** could be written that calculates a cost function (basically a goodness of fit score) based on weighted sums of reverberation, reverberation slope, and transmission loss. In fact, any other relevant parameter that could have a bearing on the overall fit could be included in the overall cost function.

8. Program File Locations

This section provides the locations of the main programs used in the course of this project.

BREVER

The current version of the **BREVER** code is located on the computers *Tessie*, *Spray*, and *Pinta* in the directory `~calnan/IDL_code/BREVER`. At the time of this writing **BREVER** consists of about 40 individual IDL routines.

Users should be aware that a number of IDL functions in this directory have names that appear in other directories, `read_dat_dat32.pro`, for example. Some of these routines are identical but others are not. Initially the same routines were copied from directory to directory so that any given directory would contain everything it needs. This is still the case, but some of the routines have been edited according to the requirements of the main program they support. In the majority of cases the changes were enhancements rather than changes in functionality, but these changes occasionally necessitated altering the parameters passed to the functions. The ultimate intent is to have the contents of every same-name function identical regardless of where they appear, but this has not yet been done.

The reason for this explanation is to warn users that if they copy **BREVER's** code from the location appearing above, they should copy all the files in that directory and not just the ones that they don't already have. The versions they may already have could have come from a different directory and so be different from the ones used by **BREVER**.

DMOS

The current versions of the *DMOS* executables are located on *Spray* and *Pinta* in the directory `/home/local/models/dmos/bin`, and on *Tessie* in the directory `~calnan/projects/RevInv/dmos/bin`. On *Tessie*, however, the executables will be moved to `/local/models/DMOS/bin` once sufficient testing has been performed and the author and Scientific Authority are satisfied that *DMOS* is working properly.

Most *DMOS* executables were produced by the GNU **g77** compiler for Intel-based Linux, but if a user needs to compile the programs for a different platform the programs' source code is located in directories near the executables, with each program's code in a separate directory. The program **BellhopDRDC_S** is a Fortran 90/95 routine that may be compiled with the **gfortran** compiler.

BellhopDMOS, however, must be compiled with **g95** due to binary file format considerations.

Speciation has also occurred with some source code files used by multiple *DMOS* programs, as it has in the IDL code and for the same reasons. Once again the intent is that ultimately the routines will be “rationalized,” but for now if a user copies the source code in order to produce a new executable, care must be taken to use only the code in that program’s subdirectory.

CASS and ER_CONV

A current executables of **CASS** and **ER_CONV** may be found on *Tessie* and *Spray* in `~calnan/bin` and on *Pinta* in `/home/local/models/dmos/bin`; in all locations the **CASS** executable is named **CASS**. The *Pinta* location is more for convenience sake than anything else since **CASS** is not a member of *DMOS*. *Tessie* has version 4 of **CASS** but the other two locations have version 3.

SAPLOT

The current version of **SAPLOT** is on *Tessie* in `/local/models/IDL-SAPLOT` and on both *Pinta* and *Spray* in `~calnan/IDL_code/SAPLOT`.

Appendix

The appendix contains the listings of the main **BREVER** output files from Runs 4, 5, and 7. They are presented primarily to present the geoacoustical parameter values that the program found to produce the best results under the constraints given to the analysis runs.

A.1 Run 4 Main BREVER Output File

Listing 3. Run 4 Main BREVER Output File

```
BASE 04 Run

Transmission loss model: CASS

ASSA Parameters:
Initial temperature: 1.00000
Temperature scaling factor: 0.990000
Number of temp. reductions: 200
Pert/temp multiplier: 5
No. downhill simplex steps: 70
No. of averaging data sets: 20000
Perturbations/temperature: 5
Perturbation value code: 1 - factor * mean of prev. 20000 pert. values
Pert. value code multiplier: 3.00000
SSA convergence value: 0.01000000
Downhill simplex conv. value: 1.00000e-04
Reverberation data weight: 1.00000
Reverberation slope weight: 0.0500000

Target Parameters:
Beam noise: is to be solved for
Beam 1 will vary from -300.000 through 200.000 dB
Beam 2 will vary from -300.000 through 200.000 dB
Beam 3 will vary from -300.000 through 200.000 dB
Beam 4 will vary from -300.000 through 200.000 dB
Beam 5 will vary from -300.000 through 200.000 dB
Beam 6 will vary from -300.000 through 200.000 dB
Points/radial: 11
CASS parameters:
Density: will vary from 1.50000 through 2.50000
Sound speed ratio: will vary from 0.500000 through 2.50000
Scattering strength: will vary from -35.0000 through -20.0000
Depth uncertainty: 0.0 m, use provided bathymetry data

Radial information:
Length: 30.0000 km
Number of radials: 6
Radial Bearings: 57.600 deg True
                           90.800 deg True
```

```

                                119.800 deg True
                                276.200 deg True
                                305.200 deg True
                                338.400 deg True

Source parameters:
Latitude:                      36.3053 N
Longitude:                     14.7192 E
Depth:                          66.0000 m
Heading:                        18.0000 deg True
Speed:                          2.50000 m/s

Receiver Parameters:
Latitude:                      36.3053 N
Longitude:                     14.7192 E
Depth:                          66.0000 m
Heading:                        18.0000 deg True

Wind Speed:                    7.50000 kt

DMOS program input filenames:
INTEGRATE:                     integrate.input
MONOGO:                         R4monogo_0576.input
                                  R4monogo_0908.input
                                  R4monogo_1198.input
                                  R4monogo_2762.input
                                  R4monogo_3052.input
                                  R4monogo_3384.input
CMBRAD:                         cmbrad.input

CASS Control Parameters:
Minimum range:                  0.100000 km
Range step size:                0.0500000 km
Start angle for rays:          -30.0000 deg
End angle for rays:            30.0000 deg
Ray angle step size:           0.0500000 deg
Max. no. of btm ray bouces:   50

Measured data filename:        R4meas_dataB.rev
No. of measured data values:  71

Reverberation data time parameters in seconds:
Minimum time:                  4.0000000
Maximum time:                   39.0000000
Time Increment size:           0.50000000

*****
11 points/radial
3.00000 km between radial points

SSA convergence did not occur before the temperature loop ran to its
limit of 200 runs. Final values are
SSA convergence value: 0.01000000
Emin:                      2175.6054
Emax:                      3067.8058

```

Convergence ratio: 0.34031297				
The downhill convergence value was not reached before its loop ran to its limit of 70 runs. The final values are				
DHS Convergence value: 1.00000e-04				
Emin: 1964.1953				
Emax: 13189.037				
Convergence ratio: 1.4815112				
Total number of DMOS runs is 4333				
Minimum E = 1964.1953				
Minimum E/radial point = 32.1999				
Best parameter estimates are:				
Beam noise results:				
Beam 1: -300.000 dB				
Beam 2: 42.783 dB				
Beam 3: -80.257 dB				
Beam 4: -38.797 dB				
Beam 5: 4.606 dB				
Beam 6: -300.000 dB				
Radial	Point	Density	Sound Speed Ratio	Scattering Strength

	Centre	2.0995	0.8059	-35.0000
1	2	2.3552	0.5000	-23.1755
1	3	1.7093	0.7127	-31.9971
1	4	2.0093	1.1433	-31.8976
1	5	1.8712	2.1024	-20.7178
1	6	1.7960	1.2966	-26.5868
1	7	2.1076	1.9595	-20.3916
1	8	1.5000	2.1379	-21.2755
1	9	1.8515	2.1905	-25.8285
1	10	2.2888	1.9761	-24.0872
1	11	1.6756	1.2493	-32.0698
2	2	1.6175	0.5000	-30.5679
2	3	1.8386	1.1205	-23.8244
2	4	2.3618	1.1202	-30.5763
2	5	2.2672	2.0596	-20.0000
2	6	1.6374	2.5000	-26.7478
2	7	2.3753	2.2654	-27.9824
2	8	1.8116	1.3873	-21.4116
2	9	2.4485	2.1378	-23.8079
2	10	1.6375	1.1763	-24.2414
2	11	2.2515	1.4701	-29.6515
3	2	2.1572	2.0015	-29.5816
3	3	1.8292	0.9434	-35.0000
3	4	1.8365	1.7301	-25.4090
3	5	2.4010	0.6625	-23.3956
3	6	2.2267	2.3443	-20.0864
3	7	1.7716	1.6178	-21.1013
3	8	2.0608	1.5392	-27.4893

3	9	1.7701	2.3205	-26.3587
3	10	1.6984	1.7046	-23.9942
3	11	2.4651	1.5964	-29.9577
4	2	2.5000	0.9098	-27.6974
4	3	1.8314	0.6642	-33.0910
4	4	1.9959	2.0906	-26.3085
4	5	1.9936	1.8320	-29.5252
4	6	2.4228	1.1389	-24.6336
4	7	2.5000	2.0300	-35.0000
4	8	1.8255	0.5554	-22.2592
4	9	1.7139	0.7415	-21.2093
4	10	1.8281	2.5000	-31.2220
4	11	1.9529	2.1796	-28.2937
5	2	1.6139	1.6818	-33.3726
5	3	1.8978	0.5259	-26.9541
5	4	2.4089	1.5521	-32.7616
5	5	2.3697	0.7096	-32.9960
5	6	1.6452	1.3356	-22.3697
5	7	1.8206	2.4422	-34.4766
5	8	2.3733	1.0369	-31.2321
5	9	1.7294	2.2641	-28.7093
5	10	2.0705	1.2429	-27.7976
5	11	1.5000	2.4204	-28.1904
6	2	1.5695	0.5000	-23.5214
6	3	2.1559	0.5103	-25.4679
6	4	2.0390	1.3646	-34.3783
6	5	1.8226	0.7396	-30.8681
6	6	2.1727	0.9582	-33.6384
6	7	2.0726	2.1762	-32.6578
6	8	2.0471	0.7397	-21.2987
6	9	1.6130	1.3052	-34.1746
6	10	2.4607	2.1368	-22.4587
6	11	2.2741	0.5000	-34.9297

Analysis started: Thu Apr 20 19:10:57 2006
 Analysis ended: Sat Apr 22 17:48:14 2006
 Duration of analysis run: 1 days 22:37:17

A.2 Run 5 Main BREVER Output File

Listing 4. Run 5 Main BREVER Output File

```
BASE 04 Run

Transmission loss model: CASS

ASSA Parameters:
Initial temperature: 1.00000
Temperature scaling factor: 0.990000
Number of temp. reductions: 200
Pert/temp multiplier: 5
No. downhill simplex steps: 70
No. of averaging data sets: 20000
Perturbations/temperature: 5
Perturbation value code: 1 - factor * mean of prev. 20000 pert. values
Pert. value code multiplier: 3.00000
SSA convergence value: 0.01000000
Downhill simplex conv. value: 1.00000e-04
Reverberation data weight: 1.00000
Reverberation slope weight: 0.0500000

Target Parameters:
Beam noise: is to be solved for
Beam 1 will vary from -300.000 through 200.000 dB
Beam 2 will vary from -300.000 through 200.000 dB
Beam 3 will vary from -300.000 through 200.000 dB
Beam 4 will vary from -300.000 through 200.000 dB
Beam 5 will vary from -300.000 through 200.000 dB
Beam 6 will vary from -300.000 through 200.000 dB
Points/radial: 17
CASS parameters:
Density: will vary from 1.50000 through 2.50000
Sound speed ratio: will vary from 0.500000 through 2.50000
Scattering strength: will vary from -35.0000 through -20.0000
Depth uncertainty: 0.0 m, use provided bathymetry data

Radial information:
Length: 8.00000 km
Number of radials: 6
Radial Bearings:
57.600 deg True
90.800 deg True
119.800 deg True
276.200 deg True
305.200 deg True
338.400 deg True

Source parameters:
Latitude: 36.3053 N
Longitude: 14.7192 E
Depth: 66.0000 m
Heading: 18.0000 deg True
```

Speed:	2.50000 m/s
Receiver Parameters:	
Latitude:	36.3053 N
Longitude:	14.7192 E
Depth:	66.0000 m
Heading:	18.0000 deg True
Wind Speed:	7.50000 kt
DMOS program input filenames:	
INTEGRATE:	R5integrate.input
MONOGO:	R5monogo_0576.input R5monogo_0908.input R5monogo_1198.input R5monogo_2762.input R5monogo_3052.input R5monogo_3384.input
CMBRAD:	R5cmbrad.input
CASS Control Parameters:	
Minimum range:	0.100000 km
Range step size:	0.0500000 km
Start angle for rays:	-30.0000 deg
End angle for rays:	30.0000 deg
Ray angle step size:	0.0500000 deg
Max. no. of btm ray bounces:	50
Measured data filename:	R5meas_dataB.rev
No. of measured data values:	17
Reverberation data time parameters in seconds:	
Minimum time:	2.000000
Maximum time:	10.000000
Time Increment size:	0.50000000

17 points/radial	
0.500000 km between radial points	
SSA convergence did not occur before the temperature loop ran to its limit of 200 runs. Final values are	
SSA convergence value:	0.01000000
Emin:	1132.6889
Emax:	1233.7845
Convergence ratio:	0.085439878
The downhill convergence value was not reached before its loop ran to its limit of 70 runs. The final values are	
DHS Convergence value:	1.00000e-04
Emin:	1113.8326
Emax:	3043.4061
Convergence ratio:	0.92829571
Total number of DMOS runs is	2666

Minimum E	=	1113.8326
Minimum E/radial point	=	11.4828
Best parameter estimates are:		

Beam noise results:

Beam 1:	-166.477 dB
Beam 2:	-263.837 dB
Beam 3:	-300.000 dB
Beam 4:	-17.843 dB
Beam 5:	-300.000 dB
Beam 6:	-253.398 dB

Radial	Point	Density	Sound Speed Ratio	Scattering Strength
<hr/>				
Centre		1.5000	1.8951	-35.0000
1	2	2.5000	1.9246	-32.8882
1	3	1.6311	1.5279	-21.5136
1	4	1.9886	1.6234	-27.4198
1	5	1.7760	0.9250	-29.8988
1	6	2.1982	1.3420	-32.8359
1	7	2.3602	1.8153	-20.0000
1	8	1.8005	1.0786	-26.1080
1	9	1.9737	1.1076	-29.0133
1	10	2.3828	0.8160	-31.1652
1	11	1.9192	0.8141	-21.3952
1	12	1.6411	0.5425	-34.1316
1	13	2.1818	0.5000	-20.2257
1	14	2.4449	2.0642	-24.3385
1	15	2.3553	1.5500	-23.5513
1	16	2.1341	1.8018	-27.2020
1	17	2.0041	2.2529	-30.3745
2	2	2.0588	1.8134	-26.5573
2	3	2.4687	2.2047	-21.9761
2	4	2.0695	1.9826	-33.9350
2	5	1.8669	1.4133	-27.7888
2	6	1.6984	1.1571	-33.6520
2	7	2.2565	1.6453	-33.3085
2	8	2.0893	1.4599	-23.4044
2	9	2.3588	1.0098	-33.9940
2	10	2.2204	0.7965	-28.7564
2	11	1.9181	2.2520	-30.4407
2	12	1.5994	1.2024	-20.0000
2	13	2.3421	1.5141	-29.3064
2	14	2.4262	0.5547	-27.5999
2	15	1.9919	1.1872	-28.9028
2	16	2.0880	1.9950	-35.0000
2	17	2.5000	0.9246	-20.0000
3	2	1.9978	2.2519	-28.4690
3	3	2.1856	1.0061	-29.6943
3	4	1.5000	2.1107	-22.6424
3	5	1.6896	0.8711	-25.6779
3	6	1.5421	0.8991	-35.0000

3	7	2.0469	1.0539	-21.6962
3	8	2.2901	0.5000	-31.7282
3	9	1.6014	1.0329	-23.4291
3	10	2.0511	0.5000	-21.0462
3	11	1.5748	1.1827	-32.5087
3	12	1.5743	2.1142	-25.6983
3	13	2.1819	1.2564	-26.5504
3	14	2.5000	1.5688	-27.7547
3	15	2.2002	0.8315	-31.9120
3	16	2.1131	0.5000	-30.1584
3	17	2.0623	0.9667	-34.7906
4	2	1.8106	1.0110	-28.5575
4	3	2.0824	0.9370	-33.7093
4	4	1.8314	2.1794	-20.0000
4	5	1.8154	1.8369	-32.8407
4	6	1.8779	2.3051	-23.5133
4	7	1.7409	1.3681	-26.4666
4	8	1.5754	1.9614	-27.4311
4	9	1.6021	2.3031	-21.0741
4	10	2.4116	0.7069	-35.0000
4	11	2.1744	2.2756	-28.1227
4	12	2.2763	1.5269	-30.7358
4	13	1.6637	1.9904	-28.5581
4	14	2.0443	1.2453	-32.0747
4	15	2.1438	1.5394	-22.0332
4	16	2.2593	0.6020	-21.4736
4	17	2.0888	1.8564	-33.2579
5	2	2.4264	1.3084	-25.1129
5	3	1.7788	1.6843	-23.5544
5	4	1.5222	2.0053	-32.8160
5	5	2.1927	1.1570	-33.9442
5	6	1.6407	1.7632	-33.7717
5	7	1.9247	2.3746	-34.0117
5	8	2.0748	0.7225	-28.6787
5	9	1.5792	1.1496	-20.1308
5	10	2.1313	1.8668	-21.5878
5	11	2.2570	0.9824	-22.2187
5	12	2.2172	0.8417	-24.8195
5	13	2.1681	2.0612	-27.1157
5	14	1.5472	0.5856	-24.3125
5	15	1.9813	1.0169	-20.2454
5	16	2.1487	0.5738	-29.5770
5	17	1.9439	2.0253	-31.0434
6	2	1.6196	0.9519	-33.1116
6	3	2.2590	1.3567	-27.4507
6	4	2.2845	1.8570	-26.8204
6	5	2.1216	0.8660	-24.4641
6	6	2.0437	0.5000	-26.4136
6	7	1.5291	1.7291	-26.6129
6	8	1.6451	1.4911	-32.1361
6	9	2.1534	2.3992	-25.6196
6	10	1.5116	1.7989	-26.7406
6	11	1.5506	0.9235	-34.1988

6	12	2.0515	1.5562	-30.2479
6	13	2.3414	1.0338	-27.8832
6	14	2.1872	0.9756	-25.8303
6	15	1.7828	2.1051	-24.2498
6	16	1.8600	2.3470	-32.5012
6	17	1.8507	1.5767	-27.0944

```

Analysis started:      Sat Apr 22 17:48:14 2006
Analysis ended:       Sun Apr 23 01:39:37 2006
Duration of analysis run: 07:51:23

```

A.3 Run 7 Main BREVER Output File

Listing 5. Run 7 Main BREVER Output File

```

BASE 04 Run

Transmission loss model:          CASS

ASSA Parameters:
  Initial temperature:            1.00000
  Temperature scaling factor:    0.990000
  Number of temp. reductions:   200
  Pert/temp multiplier:         5
  No. downhill simplex steps:  70
  No. of averaging data sets: 20000
  Perturbations/temperature:   5
  Perturbation value code:     1 - factor * mean of prev. 20000 pert. values
  Pert. value code multiplier: 3.00000
  SSA convergence value:       0.01000000
  Downhill simplex conv. value: 1.00000e-04
  Reverberation data weight:   1.00000
  Reverberation slope weight:  0.0500000

Target Parameters:
  Beam noise:                   is not to be solved for but ".sys" file values
                                are to be replaced
    Beam  1:                     fixed at 44.500 dB
    Beam  2:                     fixed at 44.500 dB
    Beam  3:                     fixed at 47.000 dB
    Beam  4:                     fixed at 46.800 dB
    Beam  5:                     fixed at 44.800 dB
    Beam  6:                     fixed at 47.000 dB
  Points/radial:                11
  CASS parameters:
    Density:                    will vary from 1.50000 through 2.50000
    Sound speed ratio:          will vary from 0.800000 through 2.50000
    Scattering strength:        will vary from -35.0000 through -20.0000

```

```

Depth uncertainty:          0.0 m, use provided bathymetry data

Radial information:
Length:                  30.0000 km
Number of radials:        6
Radial Bearings:
      57.600 deg True
      90.800 deg True
      119.800 deg True
      276.200 deg True
      305.200 deg True
      338.400 deg True

Source parameters:
Latitude:                36.3053 N
Longitude:                14.7192 E
Depth:                   66.0000 m
Heading:                 18.0000 deg True
Speed:                   2.50000 m/s

Receiver Parameters:
Latitude:                36.3053 N
Longitude:                14.7192 E
Depth:                   66.0000 m
Heading:                 18.0000 deg True

Wind Speed:               7.50000 kt

DMOS program input filenames:
INTEGRATE:                R7integrate.input
MONOGO:
      R7monogo_0576.input
      R7monogo_0908.input
      R7monogo_1198.input
      R7monogo_2762.input
      R7monogo_3052.input
      R7monogo_3384.input
CMBRAD:                   R7cmbad.input

CASS Control Parameters:
Minimum range:             0.100000 km
Range step size:            0.0500000 km
Start angle for rays:       -30.0000 deg
End angle for rays:          30.0000 deg
Ray angle step size:         0.0500000 deg
Max. no. of btm ray bouces: 50

Measured data filename:     R7meas_dataB.rev
No. of measured data values: 71

Reverberation data time parameters in seconds:
Minimum time:              4.0000000
Maximum time:              39.0000000
Time Increment size:         0.50000000

*****
11 points/radial

```

3.00000 km between radial points

SSA convergence did not occur before the temperature loop ran to its limit of 200 runs. Final values are
 SSA convergence value: 0.01000000
 Emin: 2260.3419
 Emax: 3316.8062
 Convergence ratio: 0.37885468

The downhill convergence value was not reached before its loop ran to its limit of 70 runs. The final values are
 DHS Convergence value: 1.00000e-04
 Emin: 1668.5939
 Emax: 6266.7260
 Convergence ratio: 1.1589028

Total number of DMOS runs is 5047
 Minimum E = 1668.5939
 Minimum E/radial point = 27.3540
 Best parameter estimates are:

Radial	Point	Density	Sound Speed Ratio	Scattering Strength
<hr/>				
Centre		2.4358	0.8310	-35.0000
1	2	1.9890	0.8000	-22.4683
1	3	2.1575	0.8000	-30.5989
1	4	2.2498	0.8000	-35.0000
1	5	1.7914	2.1863	-34.2308
1	6	1.8957	1.6344	-20.4219
1	7	1.6121	1.7232	-23.0321
1	8	2.2628	2.2653	-27.2458
1	9	2.2396	1.5599	-29.4492
1	10	1.6652	1.3805	-34.0455
1	11	1.8435	0.8266	-33.8227
2	2	2.1555	0.9342	-31.8116
2	3	2.0854	1.4271	-35.0000
2	4	2.4219	0.8862	-22.5573
2	5	1.6887	2.1262	-29.6914
2	6	2.3660	1.1522	-23.9359
2	7	2.0440	2.1724	-34.4066
2	8	1.6700	1.3169	-33.4822
2	9	1.8108	2.4042	-24.3596
2	10	2.3064	1.4196	-21.8180
2	11	2.1732	1.9448	-35.0000
3	2	1.8706	0.8000	-32.8927
3	3	1.9762	2.1709	-26.2888
3	4	1.6933	2.2524	-32.4720
3	5	2.2385	1.4038	-24.2390
3	6	1.9359	1.9329	-22.0823
3	7	1.9306	1.9552	-33.2108
3	8	2.1140	1.4616	-34.6104
3	9	1.8005	2.0423	-20.8987

3	10	1.7824	2.1872	-30.7718
3	11	2.0895	1.6042	-30.7082
4	2	1.5765	1.0642	-25.9076
4	3	1.5000	1.7749	-30.0399
4	4	2.1236	0.8469	-27.6160
4	5	2.3248	1.8364	-27.1463
4	6	1.8698	2.5000	-25.9139
4	7	1.8288	1.3769	-32.0683
4	8	1.9349	1.2653	-20.0000
4	9	2.2543	1.5802	-34.3762
4	10	2.1966	2.0505	-25.9381
4	11	2.0384	1.3170	-20.4474
5	2	1.9715	0.8000	-34.6565
5	3	2.4445	2.1032	-25.2560
5	4	2.0787	1.1520	-23.6481
5	5	1.5484	2.4104	-24.4472
5	6	1.9899	1.4455	-24.1723
5	7	1.7398	1.7188	-21.6121
5	8	2.2799	1.5313	-26.2584
5	9	2.0197	2.2495	-20.0000
5	10	2.5000	0.9876	-24.1688
5	11	1.9273	1.6931	-20.0000
6	2	2.4641	0.8387	-34.1670
6	3	2.2125	2.2274	-30.0764
6	4	1.8437	1.2145	-27.7958
6	5	2.0003	1.2481	-32.4957
6	6	1.7883	1.2951	-34.1836
6	7	1.5371	1.3683	-22.1289
6	8	1.9053	1.4501	-24.3897
6	9	1.9477	1.3201	-27.2356
6	10	2.3350	2.3945	-35.0000
6	11	2.2467	2.3255	-20.9419

Analysis started: Thu May 11 17:43:37 2006
 Analysis ended: Sat May 13 23:11:09 2006
 Duration of analysis run: 2 days 05:27:31

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Initialisms and Acronyms

ASSA	Adaptive Simulated Simplex Annealing
CASS	Comprehensive Acoustic System Simulation
DAP	Drifting Acoustic Projector
DASM	Directional Acoustic Sensor Module
DMOS	DRDC Atlantic Model Operating System
DRDC	Defence Research and Development Canada
GRAB	Gaussian Ray Bundle
MDA	MacDonald, Dettwiler & Associates Ltd.

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(U) A previous contract resulted in the addition of the ray theory program Bellhop to the reverberation inversion program BREVER. This was done to allow inversion of reverberation results calculated from acoustic data recorded during the BASE 04 trials. However tests with Bellhop using parameters from the BASE 04 site indicated shortcomings in that program.

The current contract began with tests runs of CASS, a potential Bellhop replacement for reverberation inversions. The test results indicated that CASS would work properly for the analysis area. Accordingly, BREVER was enhanced to allow it to also use CASS, and reverberation inversion was performed. The inversion results were used to model transmission loss, and these modelled values were compared to transmission loss data calculated from measured data.

Because of this contract the BREVER User's Guide was expanded to describe the use of the CASS-enabled version of the program.

(U) Dans le cadre d'un contrat antérieur, le programme de théorie des rayons Bellhop a été ajouté au programme d'inversion des réverbérations BREVER. Cet ajout avait pour but de permettre l'inversion des résultats de réverbérations établis à partir des données acoustiques enregistrées durant les essais BASE 04. Les essais effectués avec Bellhop à partir des paramètres de l'emplacement BASE 04 ont toutefois fait ressortir des lacunes de ce programme.

La mise en application du contrat actuel a commencé par des essais de CASS, solution possible de remplacement de Bellhop pour les inversions de réverbérations. Les résultats de ces essais ont indiqué que CASS fonctionnerait correctement pour l'analyse. Le programme BREVER a donc été adapté afin de pouvoir aussi utiliser CASS, et l'inversion des réverbérations a été exécutée. Les résultats de l'inversion ont servi à modéliser l'affaiblissement de transmission, et les valeurs modélisées ont été comparées aux données d'affaiblissement de transmission établies à partir des données mesurées.

À la suite de ce contrat, on a complété le guide de l'utilisateur de BREVER en décrivant l'utilisation de la version du programme faisant appel à CASS.

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